

VOLTAGE REGULATORS

Voltage regulators provide a constant DC output voltage which is almost completely unaffected by changes in the load current, the input voltage or the temperature. They form the basis of most electronic power supplies which derive their power from AC line voltage. The input voltage to a regulator is the filtered output from a diode rectifier. The diode rectifier converts the AC supply to DC but with a large ripple voltage which is very dependent on the load current. The voltage regulator removes the ripple and provides a DC voltage which is largely independent of variations in the load resistance.

There are two main categories of regulator, linear regulator and switching regulators. The simplest linear regulator uses a resistor and a Zener diode, as described earlier, but its performance is limited and most practical linear regulators use a transistor as a control element and an amplifier to provide an error signal within a negative feedback loop. The switching regulator incorporates a high – speed switching which is controlled by a feedback loop which monitors the output voltage. The switch produces a train of pulses whose duty ratio or frequency is controlled by the feedback loop. These pulses are averaged then to provide a DC output.

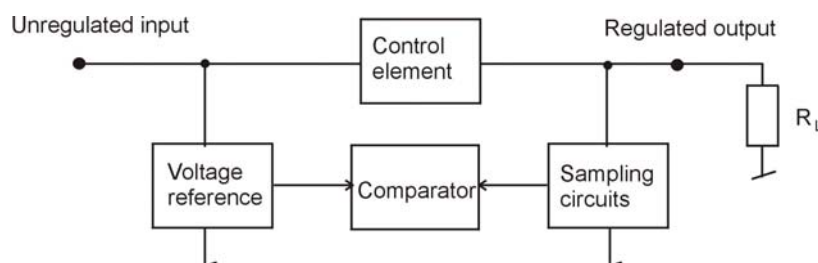
Because all mains – powered electronic equipment requires a voltage regulator, there are many linear and switching type regulators which are manufactured as integrated circuits and it is unlikely that a designer will be required to design a voltage regulator. Manufacturers' application notes provide detailed design rules for each type and the purpose of this lectures is to provide an understanding of the operating principles to enable a sensible choice to be made.

Linear regulators

The linear voltage regulator uses a transistor to regulate the flow of current and the voltage supplied to the load from an unregulated source. The purpose of the regulator is to monitor the output voltage and, by means of feedback, to maintain it as constant as possible for all load currents. Transistors can be incorporated into a regulator either as a series control element or as a shunt element.

Series regulator

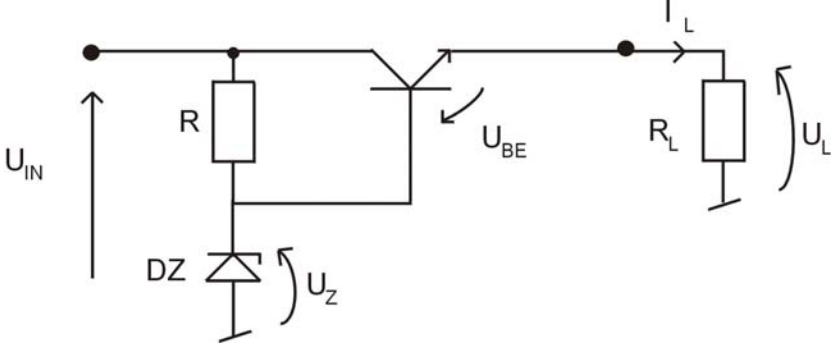
A simplified block diagram of series regulators is shown in the figure below.



Control is achieved by comparing the required output with a fixed voltage reference. If the output voltage changes, for example as a result of a variation in the load current, the input to the comparator from the sampling circuit changes in the same direction. The output generated by the comparator, resulting from the error signal, causes the control element to vary the

output voltage in the opposite direction. This action continues until the comparator detects no difference between the reference voltage and the sampled voltage.

The figure below is a circuit diagram of a simple series regulator in which the control element is an npn bipolar transistor and a Zener diode acts as the voltage reference.



The comparator function is performed by the base emitter junction which controls current flow through the transistor.

The output voltage is:

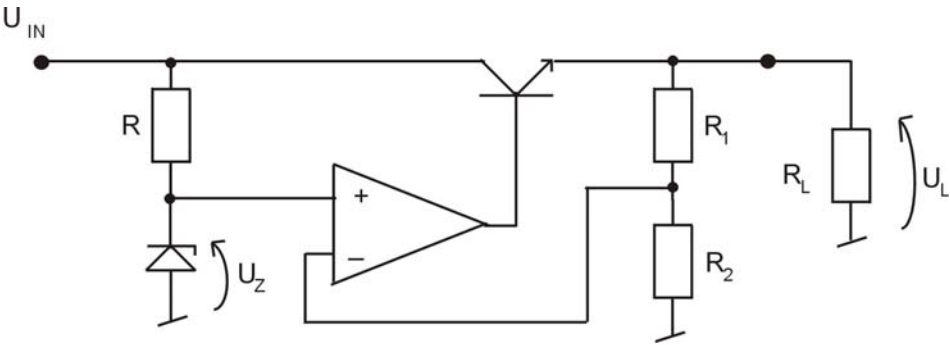
$$U_L = U_Z - U_{BE}$$

If U_L increases then U_{BE} decreases and the transistor conducts less. The reduction in the load current will cause the voltage across the load to fall, which will restore the balance.

The voltage regulation is given by the same expression as or the simple Zener diode regulator:

However, the variation of the Zener current result from the variation of the base current which is β times less than the possible change of the load current. The fact that the load current does not have to flow through R means that it can have a much larger value. Thus the regulation is greatly improved.

Further improvement in stability of the output voltage and more freedom in the choice of the Zener voltage is achieved by adding an op amp gain stage as shown in the following figure.



In this circuit the Zener voltage is more stable because the variation of the load current does not affect the Zener current. In addition, the large loop gain, resulting from the op amp, ensures that very small changes of the output voltage are detected and rapidly corrected. The output voltage settles to a value at which the input differential voltage of the op amp is almost zero so:

$$U_Z \cong U_L \frac{R_2}{R_1 + R_2}$$

Then the output voltage is:

$$U_L = U_Z \left(1 + \frac{R_1}{R_2} \right)$$

And it can be easily adjusted from a minimum value of U_Z by changing the resistor ratio. The ripple rejection is improved by a factor $1 + (k_{d0} \beta)$, where k_{d0} is the open-loop gain of the amplifier and β is the feedback factor,

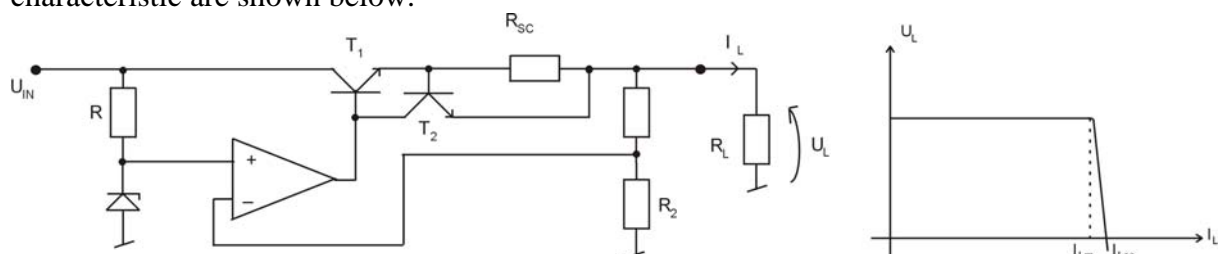
$$\beta = \frac{R_2}{R_1 + R_2}$$

The output resistance is decreased by the same factor down to a few $m\Omega$, typically.

Short – circuit protection

A serious limitation of the series regulator is that the transistor will be damaged if the output is short-circuited. Under short-circuit conditions the output current considerably increases (no feedback signal is applied to the op amp) and the full input voltage appears across the transistor. As a result the power dissipated in the transistor may increase tens of times in comparison with normal operating conditions, leading to the destruction of the transistor. Some means is thus required to limit the output short-circuit current.

A simple form of current limiter and the corresponding load current versus load voltage characteristic are shown below.



When $U_{BE2} = I_L * R_{SC}$ reaches $U_{BEF} = 0.7V$ T_2 begins to conduct heavily and consequently current which should be flowing into the base of T_1 is diverted to the collector of T_2 and thus T_1 is protected. The current through T_2 is limited by the current sourcing capability of the operational amplifier, which may be a few tens of mA.

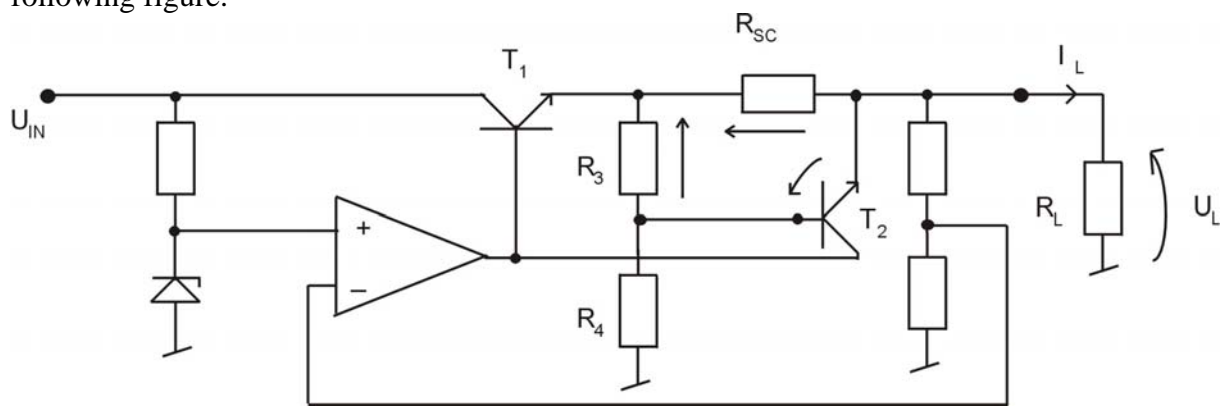
Beyond

$$I_{Lm} \cong \frac{U_{BEF}}{R_{SC}}$$

the output voltage reduces to zero with only a relatively small additional increase in current. With this protection circuit the short – circuit power dissipation in the transistor is still a few times more than under normal operating condition so to ensure reliable operation the power rating for the transistor should correspond to the short – circuit conditions.

A further development of short – circuit protection is to reduce the current as well as the voltage when a short circuit occurs.

The idea of this type of current limiting, known as fold – back current limiting, is shown in the following figure.

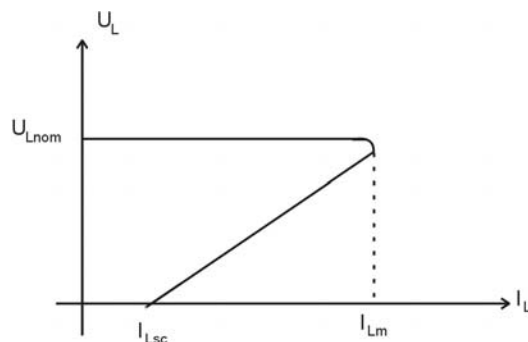


The circuit is similar to the basic, current – limiting circuit except that the base of T₂ is taken to a potential divider comprising R₃ and R₄. The base – emitter voltage of T₂ is:

$$U_{BE} = U_{R3} - U_{RSC}$$

Under normal operating conditions U_{RSC} is smaller than U_{R3} and the base – emitter junction of T₂ is reverse – biased. As the load current increases the voltage drop across R_{SC} increases more rapidly than that across R₃ until, at the maximum load current, the difference reaches U_{BEF} = 0.7V .

T₂ begins to conduct and limits the current through T₁. However, as the output voltage decreases the voltage across R₃ decreases too and then a smaller value of U_{RSC} is required to maintain U_{BE} at U_{BEF}. The reduction of U_{RSC} is achieved by a reduction in the load current. The resulting graph of load current versus load voltage is shown below.



The maximum load current I_{LM} is reached when the following condition is met:

$$U_{BE} = -(U_{Lnom} + I_{Lm} R_{SC}) \frac{R_3}{R_3 + R_4} + I_{Lm} R_{SC} = U_{BEF}$$

And from this point on the relationship between the output voltage and the load current is:

$$U_L = \frac{R_4}{R_3} I_L - U_{BEF} \left(1 + \frac{R_4}{R_3} \right)$$

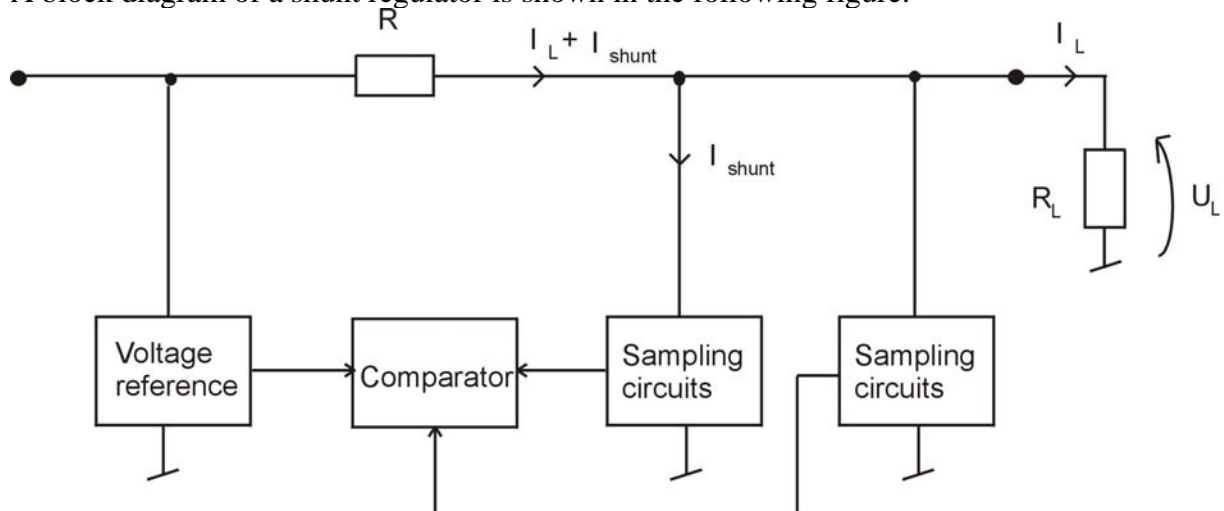
The short – circuit load current can be found by substituting $U_L=0$ and then:

$$I_{LSC} = U_{BEF} \left(1 + \frac{R_3}{R_4} \right)$$

Thanks to a considerable decrease in the short – circuit load current the short – circuit power dissipation in T_1 may even be smaller than under normal operating conditions.

Shunt regulators

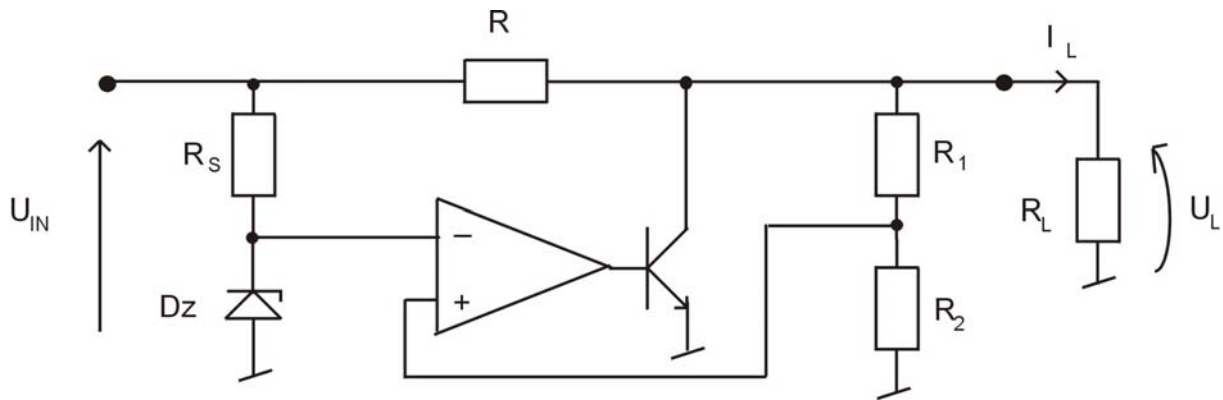
A block diagram of a shunt regulator is shown in the following figure.



As for the series regulator the current through the control element is determined by the output voltage sample which is applied to the comparator.

However, instead of controlling the load current directly, the shunt regulator bypasses current to ground. The operation of the shunt regulator is similar to that of the simple Zener diode regulator; the current through the resistor R is approximately constant and the transistor controls the distribution of this current between itself and the load.

An example circuit diagram of a shunt regulator with an operational amplifier is shown below.



One important advantage of the shunt regulator is that it is not damaged by a short – circuited output. The short – circuit current is limited to U_{IN}/R and provided the power rating for the resistor R is sufficient to withstand the short – circuit current, then there is no damage.

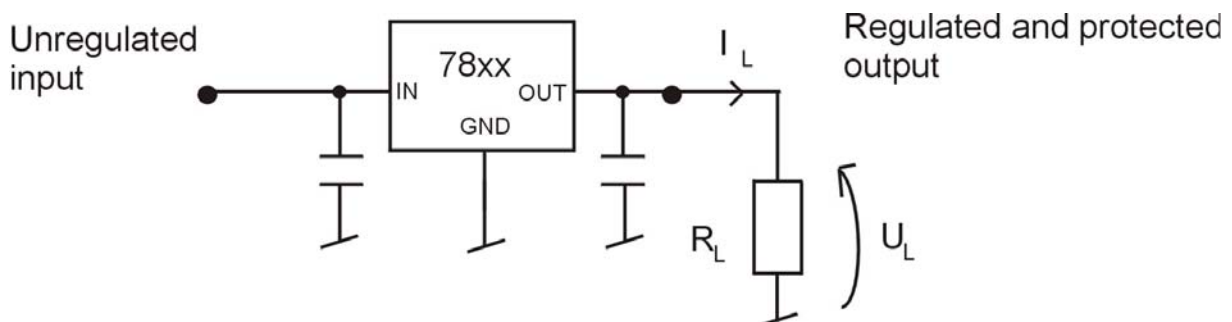
Integrated circuit regulators

For most applications it is not necessary to custom – design a voltage regulator, but rather to use any of the many “off – the – shelf” integrated circuit regulators.

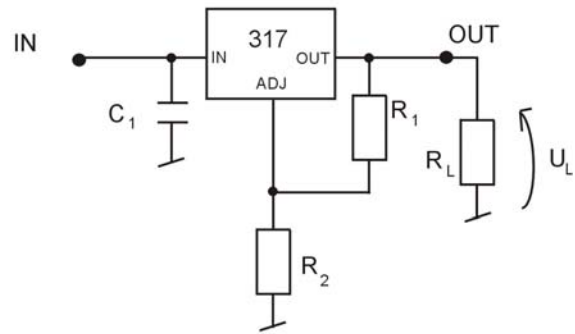
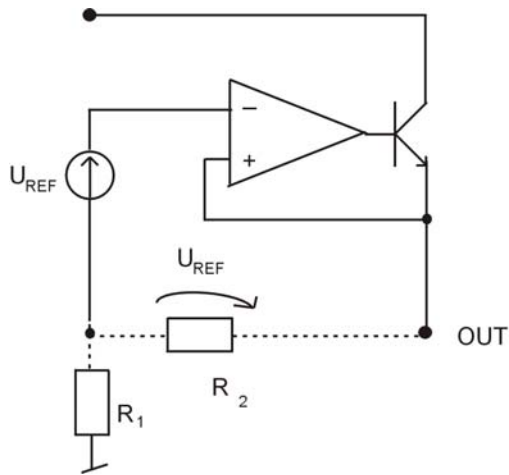
The IC regulators are available as either fixed or adjustable regulators.

Typical of fixed voltage regulators are 78xx (positive output) and 79xx (negative output), where xx is the nominal output voltage and can be any of the following: 05, 06, 08, 10, 12, 15, 18 or 24.

The application of such fixed regulators is very simple and only requires connecting two additional capacitors of at least $100\mu\text{F}$ directly to the input and to the output terminal, as shown in the figure.



Adjustable regulators are used, for example, when a nonstandard regulated voltage is required. A simplified circuit diagram of a three – terminal adjustable regulator (without protection circuits shown), of which LM317 is a classic representative, is shown below together with its application.



This regulator has no GROUND terminal. It adjust U_{OUT} to maintain a constant voltage of U_{REF} ($U_{REF} = 1.25$ for LM317) between the output terminal and the adjustment terminal. It can be easily shown that the output voltage is:

$$U_{OUT} = \left(1 + \frac{R_1}{R_2}\right) U_{REF}$$

When choosing an IC voltage regulator for a specific application the following parameters should be considered (the values in brackets are typical):

- output voltage and its tolerance (1-2%)
- minimum dropout voltage (the minimum voltage drop must be maintained between the input and the output)(0.5 – 2V)
- maximum input voltage (35 – 40V)
- maximum output current (0.1A – 5A)
- ripple rejection = $20 \log U_{\text{ripple(in)}}/U_{\text{ripple(out)}}$ (60 – 80db)
- load regulation = $(U_{L \text{ no load}} - U_{L \text{ full load}}) / U_{L \text{ no load}}$ (0.1 – 0.5%)
- line regulation (DC input rejection) = $\Delta U_L / U_{L \text{ nom}}$ for a given ΔU_{in} (0.1 – 0.2%)
- temperature stability = $\Delta U_L / \Delta U_{L \text{ nom}}$ for a given ΔT , for example 0 – 100°C
- output impedance (0.01 – 0.1Ω at low frequency of variable load current, for example 10Hz, increases with frequency).